Dynamic Van der Waals Theory

A diffuse interface model for **two-phase hydrodynamics** involving **the liquid-gas transition** in non-uniform temperature [A. Onuki, PRL (2005) & PRE (2007)]

> Hydrodynamic equations for liquid-gas flows in the bulk region [well developed]

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Boundary conditions at fluid-solid interface [J. Chem. Phys. (2010) and ongoing] Helmholtz free energy density:

$$f(n,T) = nk_BT \left[\ln \left(\lambda_{\rm th}^3 n\right) - 1 - \ln \left(1 - v_0 n\right) \right] - \varepsilon v_0 n^2$$

Internal energy density, entropy per molecule, and pressure

$$e(n,T) = 3nk_{B}T/2 - \varepsilon v_{0}n^{2}$$

$$s(n,T) = -k_{B}\ln\left[\lambda_{th}^{3}n/(1-v_{0}n)\right] + 5k_{B}/2$$

$$p(n,T) = nk_{B}T/(1-v_{0}n) - \varepsilon v_{0}n^{2}$$

Gradient contributions to the internal energy density and entropy density

$$\hat{e} = e + \frac{K(n)}{2} |\nabla n|^2 \qquad \hat{S} = ns(n, e) - \frac{C(n)}{2} |\nabla n|^2$$

Free energy minimization leads to the equilibrium structure of a diffuse liquid-gas interface. *van der Waals*

Elasticity in one-component liquid-gas systems, manifested through a reversible stress tensor $-\mathbf{\Pi}$, which is anisotropic.

Balance equations for particle number, momentum, and energy

$$\frac{\partial n}{\partial t} + \nabla \cdot (n\mathbf{v}) = 0 \quad - \text{ the continuity equation}$$
$$\frac{\partial}{\partial t} (\rho \mathbf{v}) + \nabla \cdot (\rho \mathbf{v} \mathbf{v}) = \nabla \cdot \mathbf{\vec{M}} \quad - \text{ the momentum equation}$$
$$\mathbf{\vec{M}} \equiv -\mathbf{\vec{\Pi}} + \mathbf{\vec{\sigma}} \quad \text{is the total stress tensor.}$$
$$\mathbf{reversible} \quad \text{irreversible (viscous)}$$

 $\frac{\partial \hat{e}}{\partial t} + \nabla \cdot (\hat{e}\mathbf{v}) = -\mathbf{\vec{\Pi}} : \nabla \mathbf{v} + \mathbf{\vec{\sigma}} : \nabla \mathbf{v} - \nabla \cdot \mathbf{q} \quad \text{for the internal energy density}$

Use of standard thermodynamic relations

$$\frac{\partial \hat{S}}{\partial t} + \nabla \cdot \left(\hat{S}\mathbf{v}\right) = -\nabla \cdot \hat{\mathbf{J}}_{f}^{s} + \frac{1}{T} \mathbf{\ddot{\sigma}} : \nabla \mathbf{v} - \frac{1}{T^{2}} \mathbf{q} \cdot \nabla T + \frac{1}{T} \left(-\mathbf{\ddot{\Pi}} + \hat{p}\mathbf{\ddot{I}} + M\nabla n\nabla n\right) : \nabla \mathbf{v}$$

- the balance equation for the density of entropy

 $\hat{\mathbf{J}}_{f}^{s} \equiv \left[M \nabla n \left(\partial n / \partial t + \mathbf{v} \cdot \nabla n \right) + \mathbf{q} \right] / T \quad - \text{the total entropy flux}$

The rate of entropy production in the bulk region

$$\boldsymbol{\sigma} = \frac{1}{T} \boldsymbol{\ddot{\sigma}} : \nabla \mathbf{v} - \frac{1}{T^2} \mathbf{q} \cdot \nabla T + \frac{1}{T} \left(-\boldsymbol{\ddot{\Pi}} + \hat{p} \boldsymbol{\ddot{I}} + M \nabla n \nabla n \right) : \nabla \mathbf{v}$$

The density inhomogeneity does not contribute to entropy production.

 $\begin{vmatrix} -\vec{\Pi} &= -M\nabla n\nabla n - \hat{p}\vec{I} \\ -\vec{\Pi} &= -M\nabla n\nabla n - \hat{p}\vec{I} \end{vmatrix} \quad \text{--the reversible stress}$ $\hat{p} = p - \frac{M}{2} |\nabla n|^2 + \frac{nM_n}{2} |\nabla n|^2 - Tn\nabla n \cdot \nabla \frac{M}{T} - Mn\nabla^2 n \quad \text{and} \quad M(n,T) = K(n) + C(n)T$

The positive definiteness of $\sigma = \frac{1}{T} \vec{\sigma} : \nabla \mathbf{v} - \frac{1}{T^2} \mathbf{q} \cdot \nabla T$

can be ensured by the constitutive relations

$$\vec{\sigma} = \eta \left(\nabla \mathbf{v} + \nabla \mathbf{v}^T \right) + \left(\zeta - 2\eta / 3 \right) \vec{\mathbf{I}} \nabla \cdot \mathbf{v} \qquad -\mathbf{viscous \ stress}$$
$$\mathbf{q} = -\lambda \nabla T \qquad -\mathbf{heat \ flux}$$



A schematic illustration of the fluxes into the surface region Σ_s bounded by the closed curve C_s

- No adsorption at the fluid-solid interface.
- The area densities of surface energy and surface entropy are flunctions of *n*, the boundary value of fluid density.
- Surface stress tensor and surface heat flux are present, but no surface viscosity.

The general boundary (jump) condition in differential form (a special case of the extended Kotchine's theorem)

Surface entropy and surface energy

$$\frac{\partial \phi'_s}{\partial t} + \nabla_{\tau} \cdot \left(\phi'_s \mathbf{v}_{\tau} \right) = -\nabla_{\tau} \cdot \mathbf{J}'_s + \left[\left[\hat{\boldsymbol{\gamma}} \cdot \mathbf{J} \right] \right] + \pi'_s \quad \text{with} \quad \left[\left[\hat{\boldsymbol{\gamma}} \cdot \mathbf{J} \right] \right] \equiv \hat{\boldsymbol{\gamma}} \cdot \left(\mathbf{J} - \mathbf{J}_w \right)$$

Here the prime denotes the surface quantities whose dimensions are different from the corresponding bulk quantities.

 $S_{s} = \int dA\sigma'_{s}(n) \qquad E_{s} = \int dAe'_{s}(n)$ Helmholtz free energy per unit area $f'_{s}(n,T) = e'_{s}(n) - T\sigma'_{s}(n)$ A Gibbs-type equation $d\sigma'_{s} = \frac{1}{T}de'_{s} - \frac{1}{T}\left(\frac{\partial f'_{s}}{\partial n}\right)_{T}dn$ $\gamma_{fs} = f'_{s}$ — the fluid-solid interfacial tension

Surface stress tensor is tangential and symmetric: $\vec{\mathbf{M}}'_{s} \equiv \gamma_{fs} \vec{\boldsymbol{\tau}} = f'_{s} \vec{\boldsymbol{\tau}}$ $\vec{\boldsymbol{\tau}} \equiv \vec{\mathbf{I}} - \hat{\boldsymbol{\gamma}} \hat{\boldsymbol{\gamma}}$

Balance equations at the fluid-solid interface

Force balance
$$\nabla_{\tau} f'_{s} - \hat{\mathbf{\gamma}} \cdot \mathbf{\vec{M}} + \mathbf{F} = 0 \begin{cases} \nabla_{\tau} f'_{s} - \hat{\mathbf{\gamma}} \cdot \mathbf{\vec{M}} \cdot \mathbf{\vec{\tau}} + \mathbf{F}_{\tau} = 0 \\ -\hat{\mathbf{\gamma}} \cdot \mathbf{\vec{M}} \cdot \hat{\mathbf{\gamma}} + F_{\gamma} = 0 \end{cases}$$

Three forces by the interface, fluid, and wall

Energy balance

$$\frac{\partial e'_s}{\partial t} + \nabla_{\tau} \cdot \left(e'_s \mathbf{v}_{\tau} \right) = \nabla_{\tau} \cdot \left(f'_s \mathbf{v}_{\tau} \right) - \nabla_{\tau} \cdot \mathbf{q}'_s + \left[\left[\hat{\mathbf{\gamma}} \cdot \mathbf{q} \right] \right] - \hat{\mathbf{\gamma}} \cdot \mathbf{M} \cdot \mathbf{v}_{\tau}^{slip} - \mathbf{w}_{\tau} \cdot \nabla_{\tau} f'_s$$
$$\mathbf{v}_{\tau}^{slip} = \mathbf{v}_{\tau} - \mathbf{w}_{\tau} - \text{tangential slip velocity}$$

First law of thermodynamics applied at the fluid-solid interface

Entropy balance from

$$\frac{\partial \sigma'_s}{\partial t} = \frac{1}{T} \frac{\partial e'_s}{\partial t} - \frac{1}{T} \left(\frac{\partial f'_s}{\partial n} \right)_T \frac{\partial n}{\partial t}$$

Entropy balance

$$\frac{\partial \sigma'_{s}}{\partial t} + \nabla_{\tau} \cdot \left(\sigma'_{s} \mathbf{v}_{\tau}\right) = -\nabla_{\tau} \cdot \left(\frac{\mathbf{q}'_{s}}{T}\right) + \left(\hat{\mathbf{y}} \cdot \hat{\mathbf{J}}^{s} - \hat{\mathbf{y}} \cdot \hat{\mathbf{J}}^{s}_{w}\right) + \sigma_{surf}$$
$$\hat{\mathbf{y}} \cdot \hat{\mathbf{J}}^{s} \equiv \left(\hat{\mathbf{y}} \cdot \mathbf{q} + M\dot{n}\nabla_{\gamma}n\right) / T \qquad -\hat{\mathbf{y}} \cdot \hat{\mathbf{J}}^{s}_{w} \equiv -\hat{\mathbf{y}} \cdot \mathbf{q}_{w} / T_{w} \qquad -\text{entropy fluxes}$$
$$\sigma_{surf} \equiv \mathbf{q}'_{s} \cdot \nabla_{\tau} \frac{1}{T} - \left(\frac{1}{T} - \frac{1}{T_{w}}\right) \hat{\mathbf{y}} \cdot \mathbf{q}_{w} - \frac{1}{T} \mathbf{F}_{\tau} \cdot \mathbf{v}_{\tau}^{slip} - \frac{1}{T} L\dot{n} \qquad -\text{entropy production}$$

 $L = M \nabla_{\gamma} n + (\partial f'_s / \partial n)_T$ is equal to zero in equilibrium.

Interfacial constitutive relations

$$\mathbf{q}'_{s} = -\lambda'_{s} \nabla_{\tau} T - \chi \mathbf{F}_{\tau} \qquad \kappa \hat{\mathbf{\gamma}} \cdot \mathbf{q}_{w} = -\left(\frac{1}{T} - \frac{1}{T_{w}}\right)$$
$$\beta \mathbf{v}_{\tau}^{slip} = -\beta \frac{\chi}{T} \nabla_{\tau} T - \mathbf{F}_{\tau} \qquad \alpha \dot{n} = -L$$

Balance equations (conservation laws)

Constitutive relations

Hydrodynamic equations

From the bulk region to the interface

Balance equations Constitutive relations

Hydrodynamic boundary conditions

A continuum hydrodynamic model formed by differential equations and boundary conditions.

Hydrodynamic Boundary Conditions

Density relaxation
$$\alpha \left(\frac{\partial n}{\partial t} + \mathbf{v}_{\tau} \cdot \nabla_{\tau} n \right) = -M \nabla_{\gamma} n - \left(\frac{\partial f'_s}{\partial n} \right)_T$$

Impermeability $\hat{\gamma} \cdot \mathbf{v} = \hat{\gamma} \cdot \mathbf{w} = 0$

Velocity slip $\beta \mathbf{v}_{\tau}^{slip} = -\eta \nabla_{\gamma} \mathbf{v}_{\tau} + \left[M \nabla_{\gamma} n + \left(\frac{\partial f'_s}{\partial n} \right)_T \right] \nabla_{\tau} n - \left(\sigma'_s + \beta \frac{\chi}{T} \right) \nabla_{\tau} T$

Temperature slip
$$\kappa\lambda_{w}\nabla_{\gamma}T_{w} = \frac{1}{T} - \frac{1}{T_{w}}$$
Heat fluxes
$$-\lambda\nabla_{\gamma}T + \lambda_{w}\nabla_{\gamma}T_{w} = \frac{\partial e'_{s}}{\partial t} + \nabla_{\tau} \cdot (T\sigma'_{s}\mathbf{v}_{\tau}) + \mathbf{v}_{\tau} \cdot \nabla_{\tau}f'_{s}$$

$$-\nabla_{\tau} \cdot (\lambda'_{s}\nabla_{\tau}T) - \frac{1}{\beta}\mathbf{F}_{\tau} \cdot \mathbf{F}_{\tau} - \nabla_{\tau} \cdot (\chi\mathbf{F}_{\tau}) - \frac{\chi}{T}\mathbf{F}_{\tau} \cdot \nabla_{\tau}T$$

$$\mathbf{F}_{\tau} = \eta\nabla_{\gamma}\mathbf{v}_{\tau} - M\nabla_{\gamma}n\nabla_{\tau}n - \nabla_{\tau}f'_{s} \quad \nabla_{\tau}f'_{s} = -\sigma'_{s}\nabla_{\tau}T + (\partial f'_{s}/\partial n)_{T}\nabla_{\tau}n$$

A limiting case Xu and Qian, J. Chem. Phys. 133, 204704 (2010)

No cross coupling: $\chi \to 0$ Constant temperatures at the fluid-solid interface: $T = T_w = \text{const.}$ $\kappa \to 0$ and fast relaxation toward thermal equilibrium in the solid

Density relaxation
$$\alpha \left(\frac{\partial n}{\partial t} + \mathbf{v}_{\tau} \cdot \nabla_{\tau} n \right) = -M \nabla_{\gamma} n - \left(\frac{\partial f'_s}{\partial n} \right)_T$$

Impermeability $\hat{\mathbf{\gamma}} \cdot \mathbf{v} = \hat{\mathbf{\gamma}} \cdot \mathbf{w} = 0$ Velocity slip $\beta \mathbf{v}_{\tau}^{slip} = -\eta \nabla_{\gamma} \mathbf{v}_{\tau} + \left[M \nabla_{\gamma} n + \left(\frac{\partial f'_s}{\partial n} \right)_T \right] \nabla_{\tau} n$

Dirichlet temperature condition $T = T_w = \text{const}$

